



FAMU-FSU
College of
Engineering

Design Review 5

Team 515 – Controllable CVT Device

Kemani Harris, Aaron Havener, Jacob Hernandez, Aliya Hutley,
and Cade Watson

02/18/2025

Meet Team 515



Kemani Harris
Dynamics Engineer



Aaron Havener
Controls Engineer



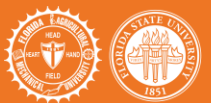
Jacob Hernandez
Design Engineer



Aliya Hutley
System Engineer & POC



Cade Watson
Materials Engineer



Sponsor & Advisor

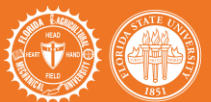
Florida Agriculture & Mechanical University and Florida State University



National Science
Foundation



Dr. Carl Moore Jr.
Associate Professor



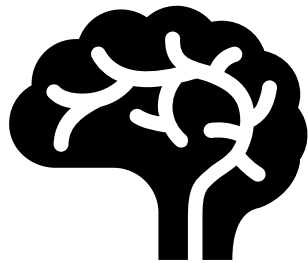
Objective

The objective of this project is to enhance the education of haptic robotics by creating a device using continuously variable transmissions (CVTs). The device is intended to utilize computer control and move through various positions to produce accurate output motion.

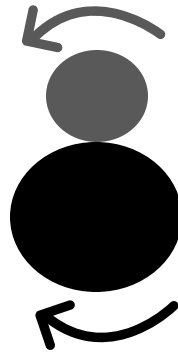


Recap

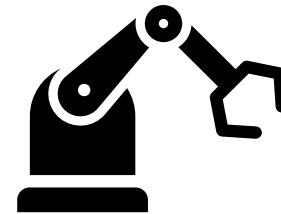
The primary goal of this project is to utilize CVT technology to present to STEM-curious students:



General autonomous robotic technology



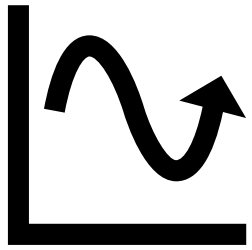
The mechanical principle of CVT's



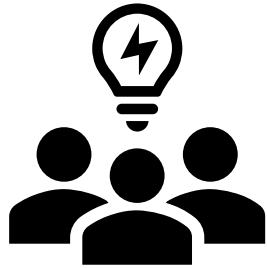
The use of CVT's in robotics

Recap

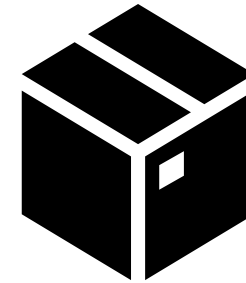
Other key design goals have been and still are:



Precise, autonomous
two-dimensional
movement



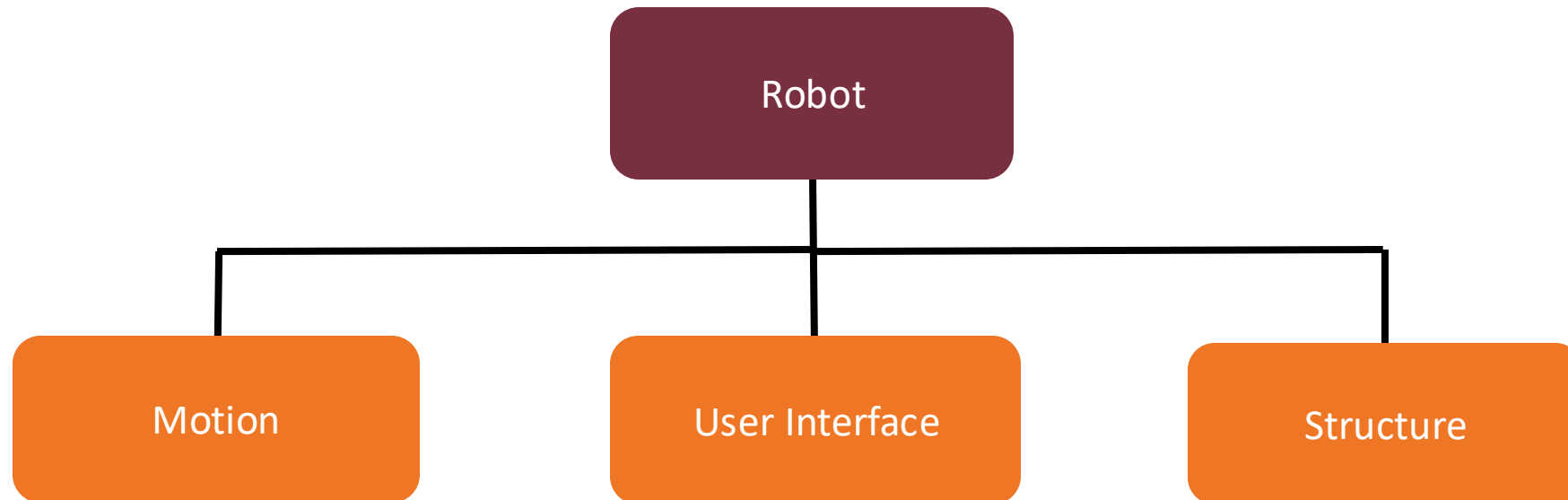
Customizable, well-
displayed, and
engaging output



Use in multiple
locations

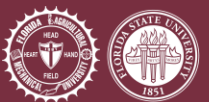
Recap

Three main systems are employed:



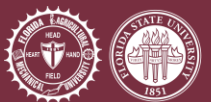
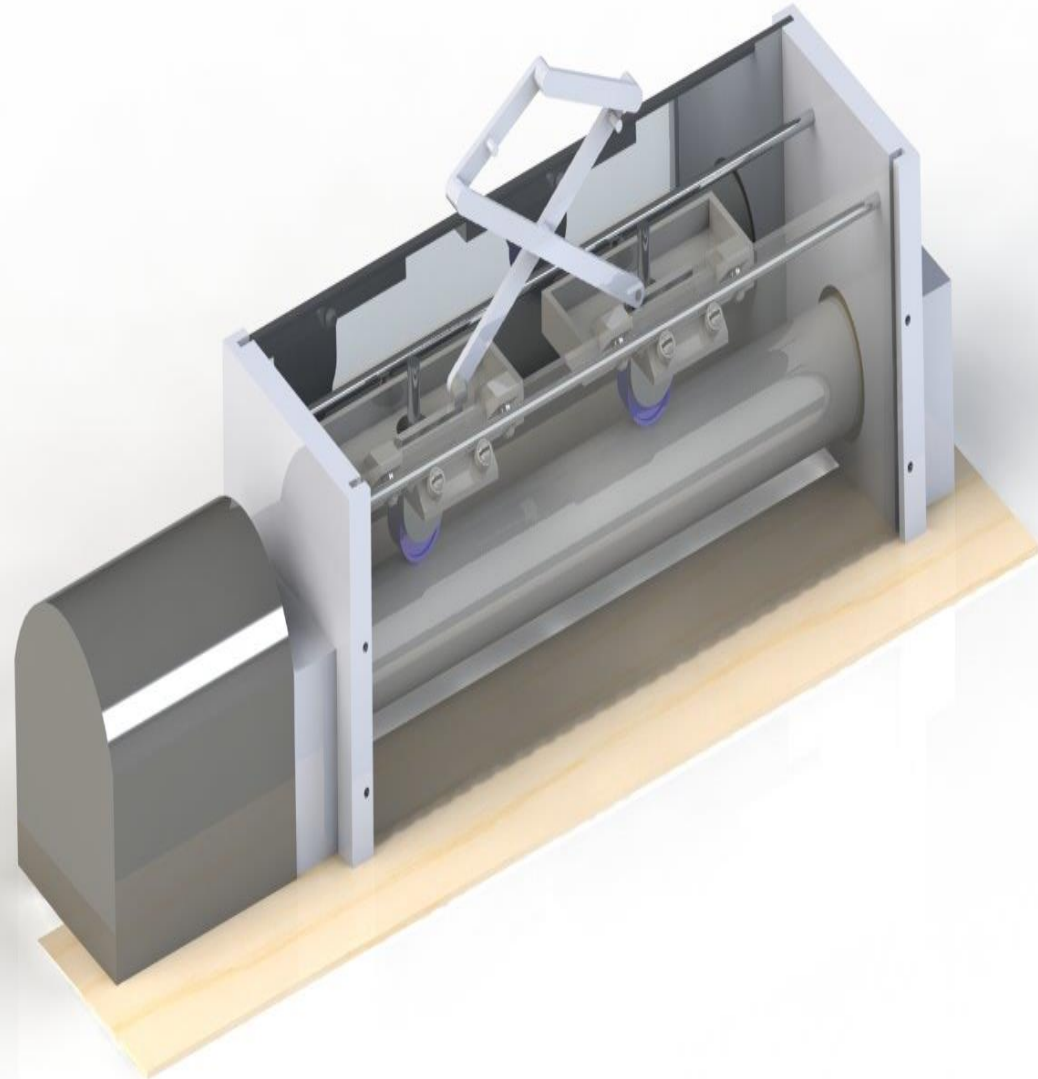
Proposed Concept

The selected concept from Fall Semester utilizes two-dimensional motion to create an interactive guessing game using light.



General Design Update

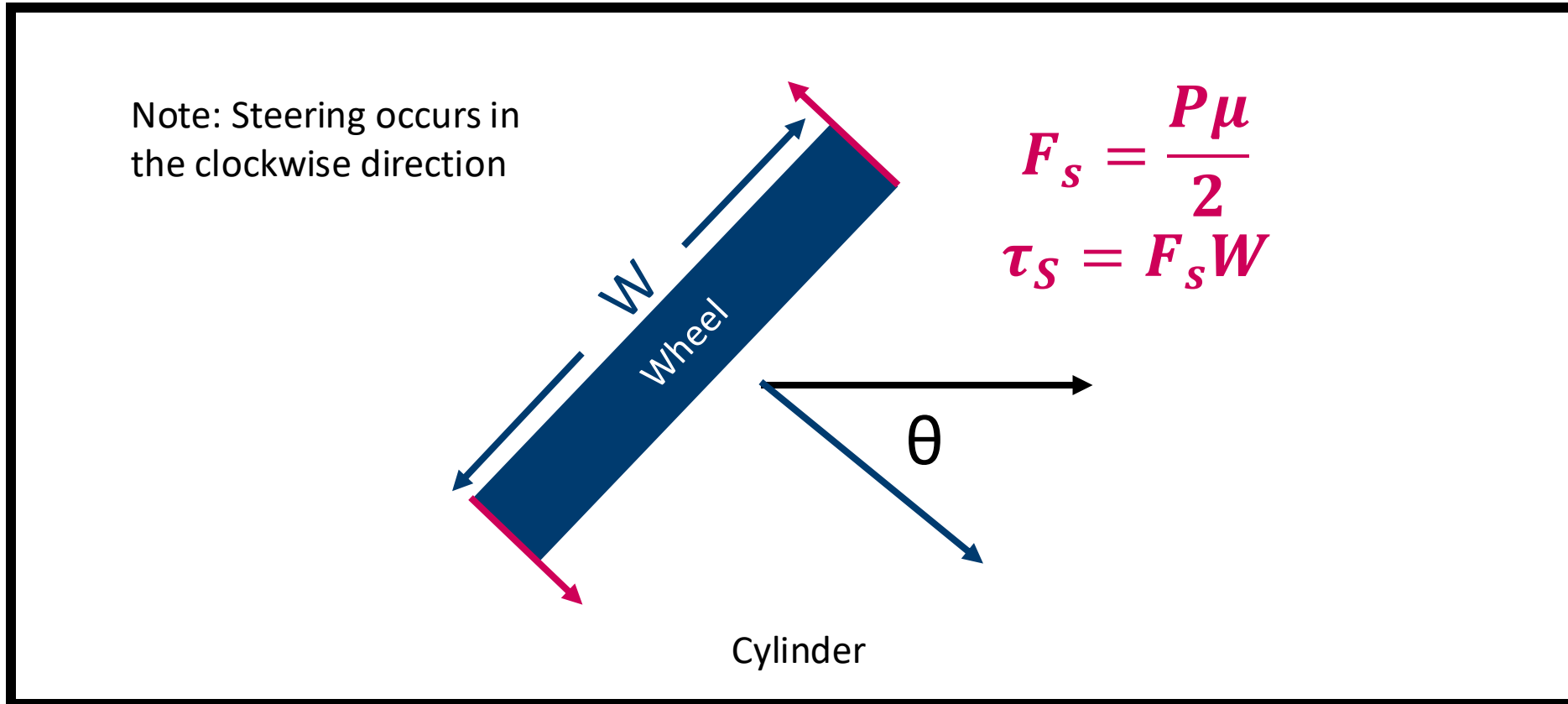
Kemani Harris



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Motion System – Steering Motor Selection

Steering motors are oversized to allow for flexibility in preload



Motion System – Steering Motor Selection

- With a maximum preload of 20 lbf, $\tau_S \approx 0.4$ Nm
- Dynamixel servo models Ax-18a and Ax-12a were compared as candidates (Ax-18a selected for higher torque and speed capabilities)

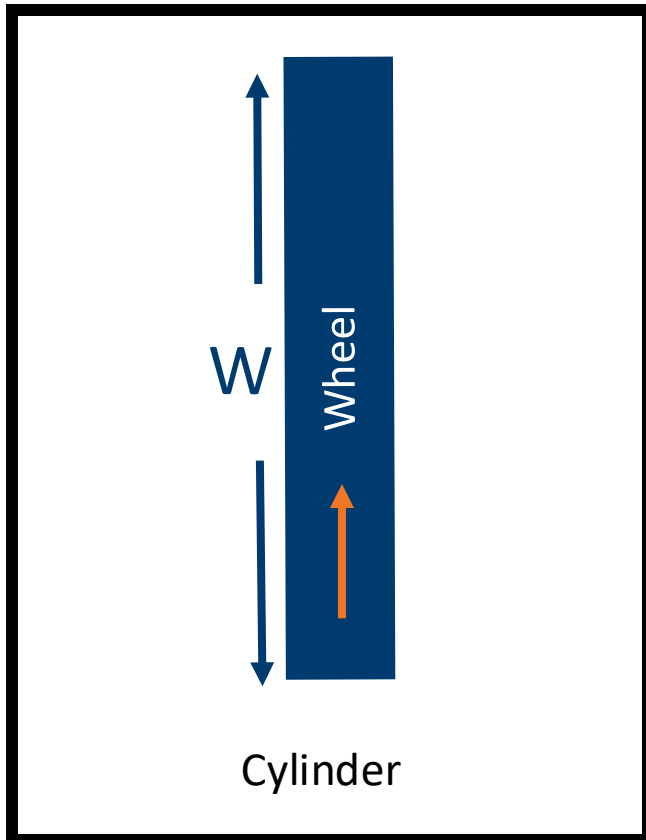


Motion System – Driving Motor Selection

Driving torque was calculated from frictional forces

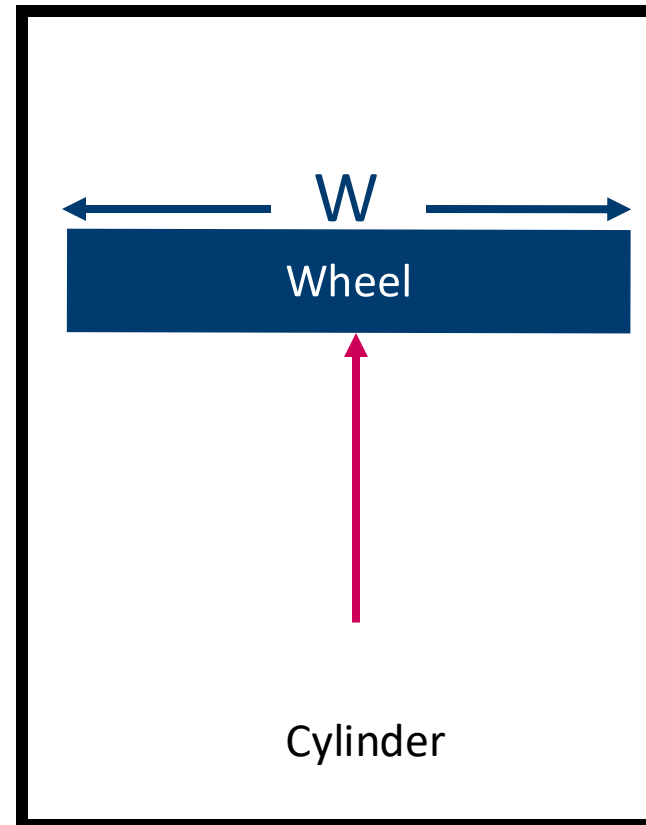
$$F_{roll} = \frac{I_{wheel}\alpha_{wheel} + b\omega_{wheel}}{r_{wheel}} \quad (small)$$
$$F_{slide} = 0$$

$\theta = 0^\circ$



$$F_{roll} = 0$$
$$F_{slide} = P\mu \quad (large)$$

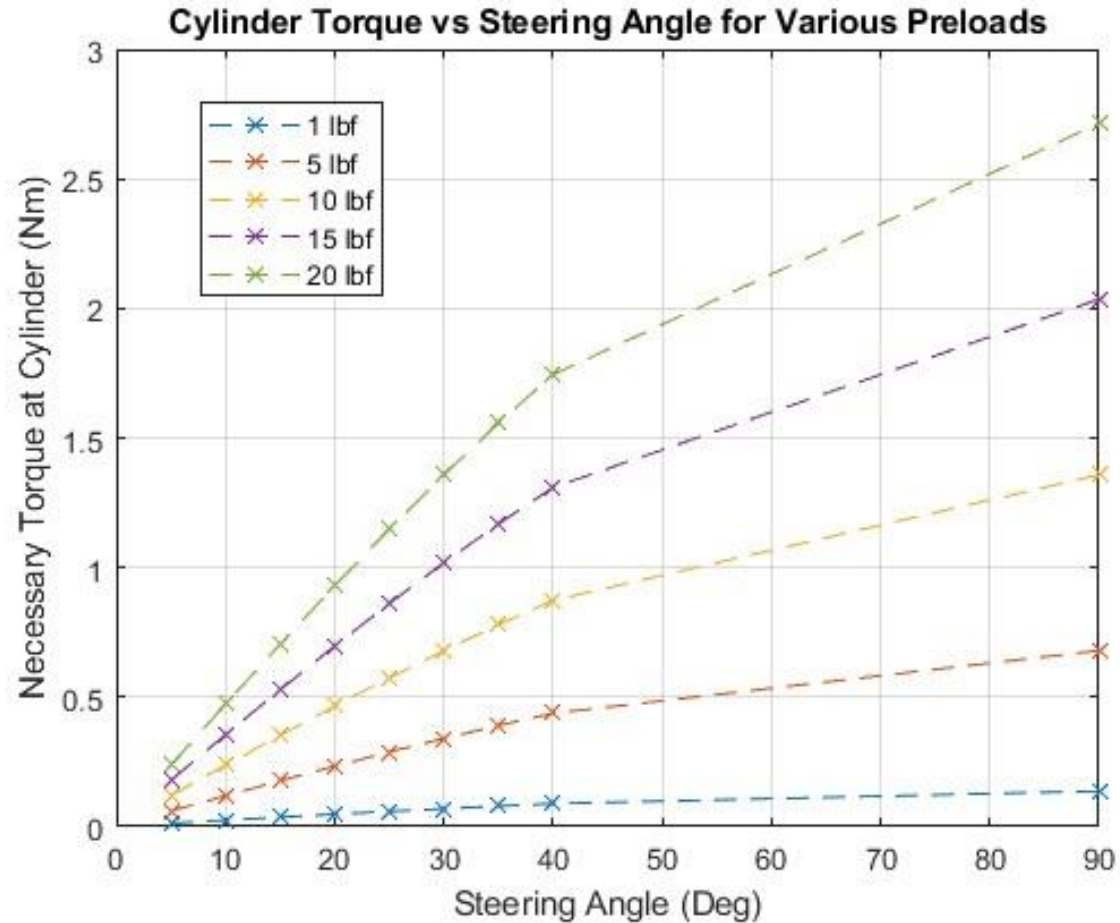
$\theta = 90^\circ$



Motion System – Driving Motor Selection

An approximation can be made for the Torque at the cylinder:

$$T_{cyl} = I_{cyl}\alpha_{cyl} + 2\mu P \sin(\theta)$$

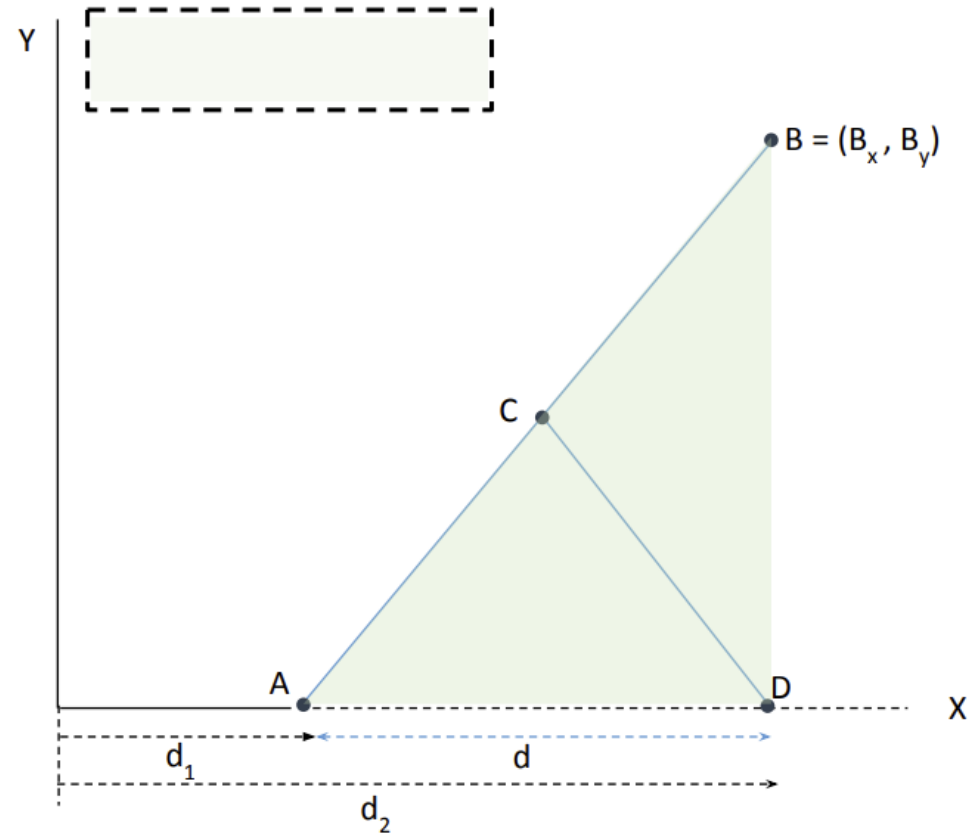


Motion System – Driving Motor Selection



- With a preload of 15 lbf at a 90° steering angle, the necessary driving torque is estimated to be around 2 Nm
- A Crouzet direct current gearmotor that can provide 2 Nm at 50 rpm is the current selected motor

Linkage Design – Prototype 0

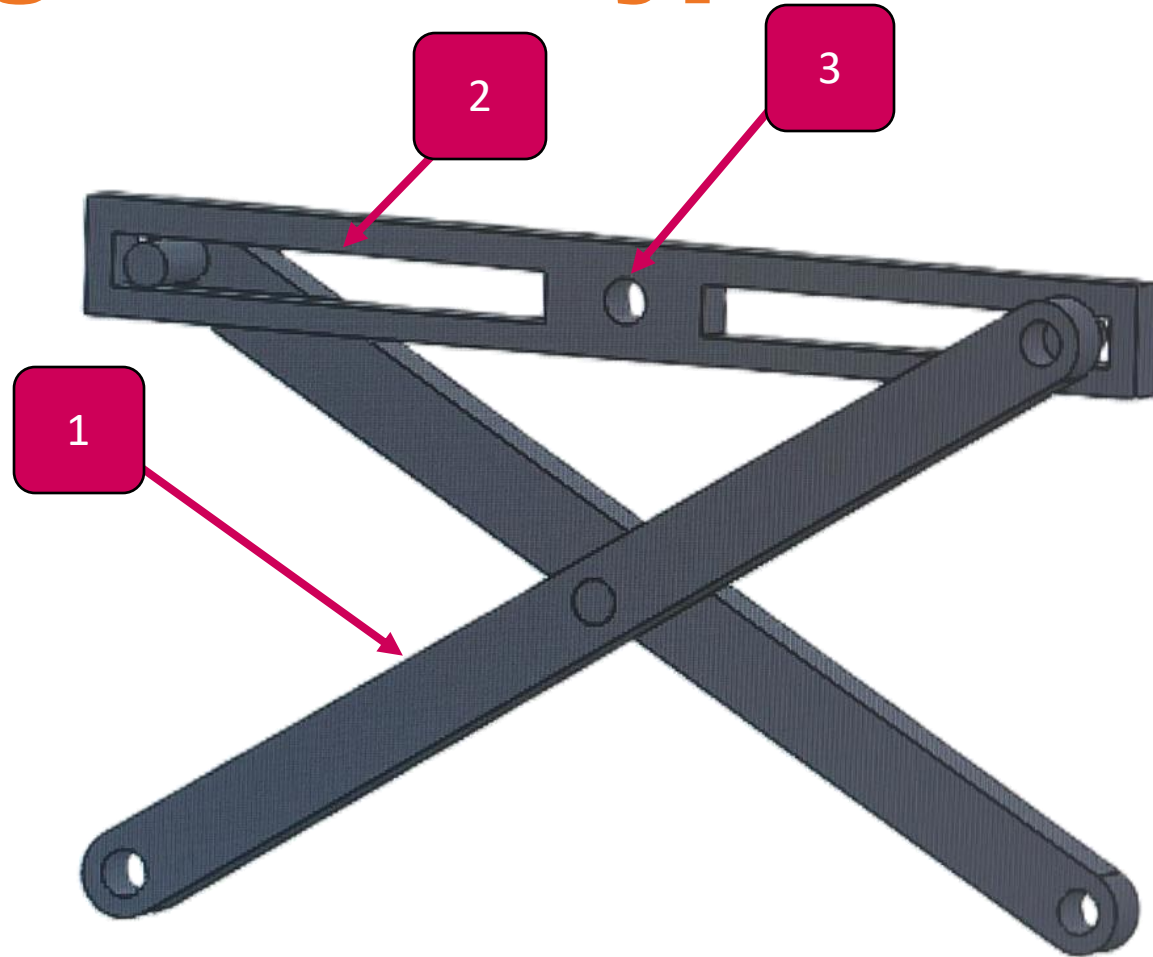


Linkage Design – Prototype 1

1) Equal Link Length

2) Slider Linkage

3) Middle Coupler Point



Linkage Design – Prototype 1

Downside

3 Degrees of Freedom

Stabilization

Waste of Resources



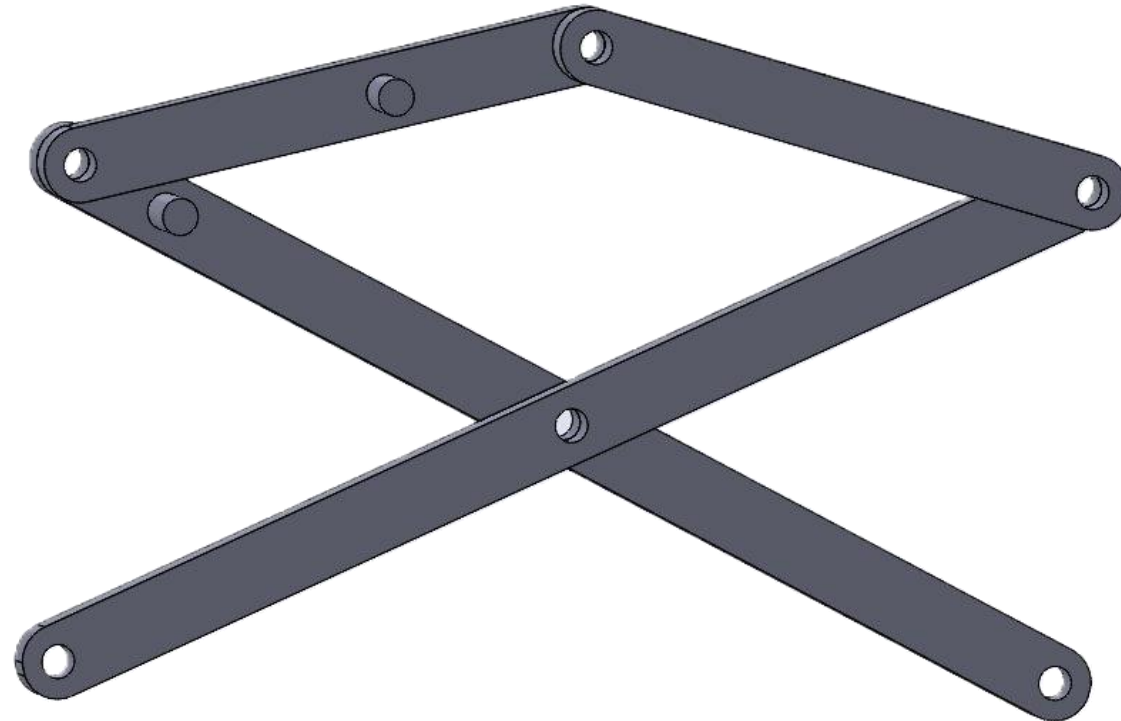
Linkage Design - Prototype 2

Smaller Link size

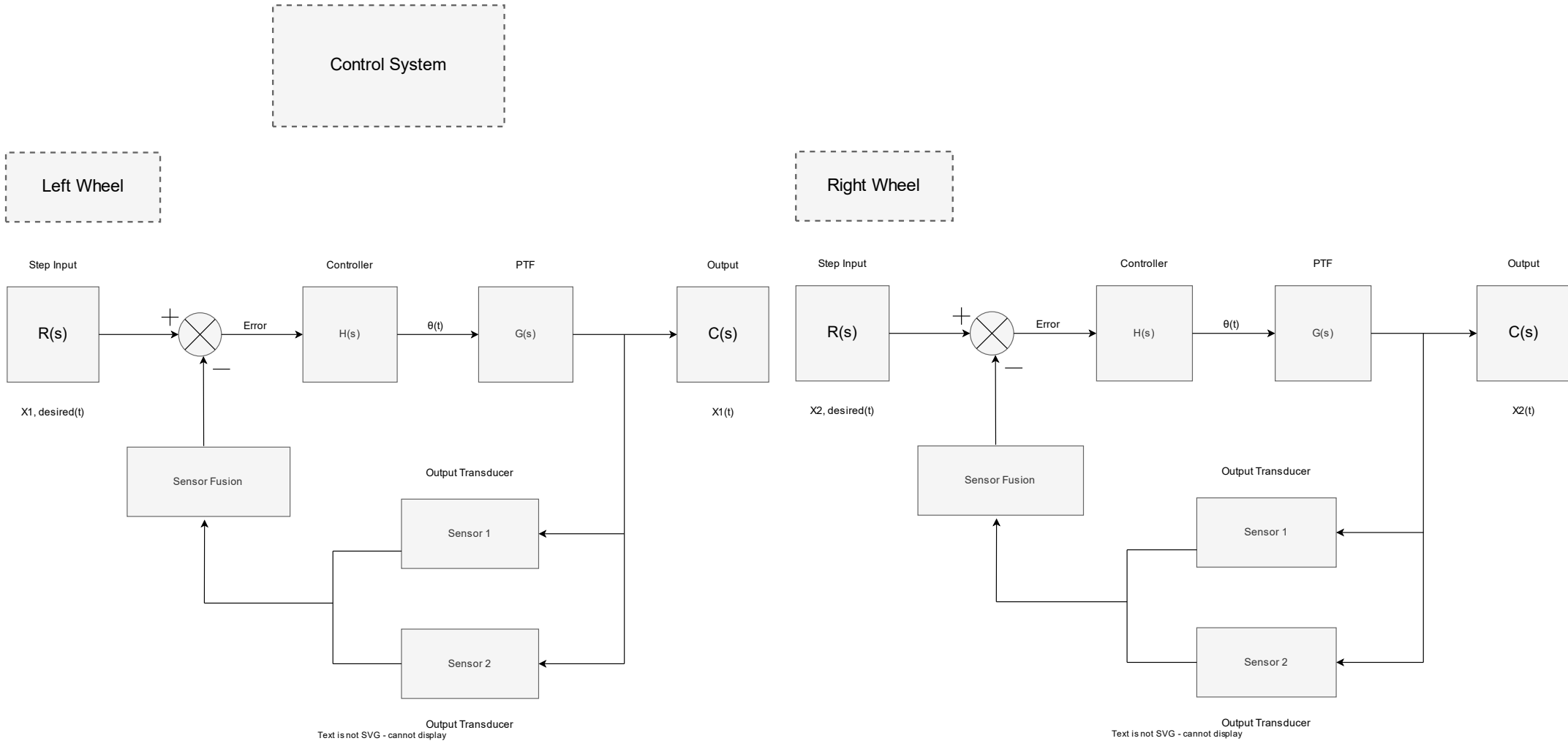
Enhances vertical motion

Reduces horizontal displacement

springs on joints



Control System Structure

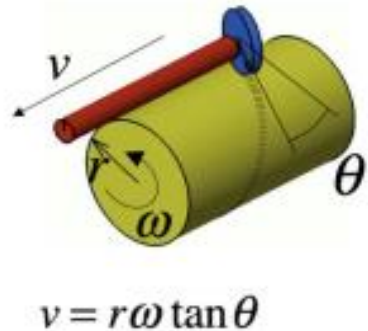


Output Transducer
Text is not SVG - cannot display

Output Transducer
Text is not SVG - cannot display



Controller Derivation



$$\frac{dx_1(t)}{dt} = v = r\omega \tan \theta$$

Control input $u(t) = \tan \theta$

$$\frac{dx_1(t)}{dt} = r\omega u(t)$$

$$sX_1(s) = r\omega U(s)$$

Plant Transfer Function $\frac{X(s)}{U(s)} = \frac{r\omega}{s}$

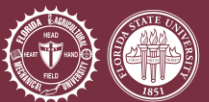
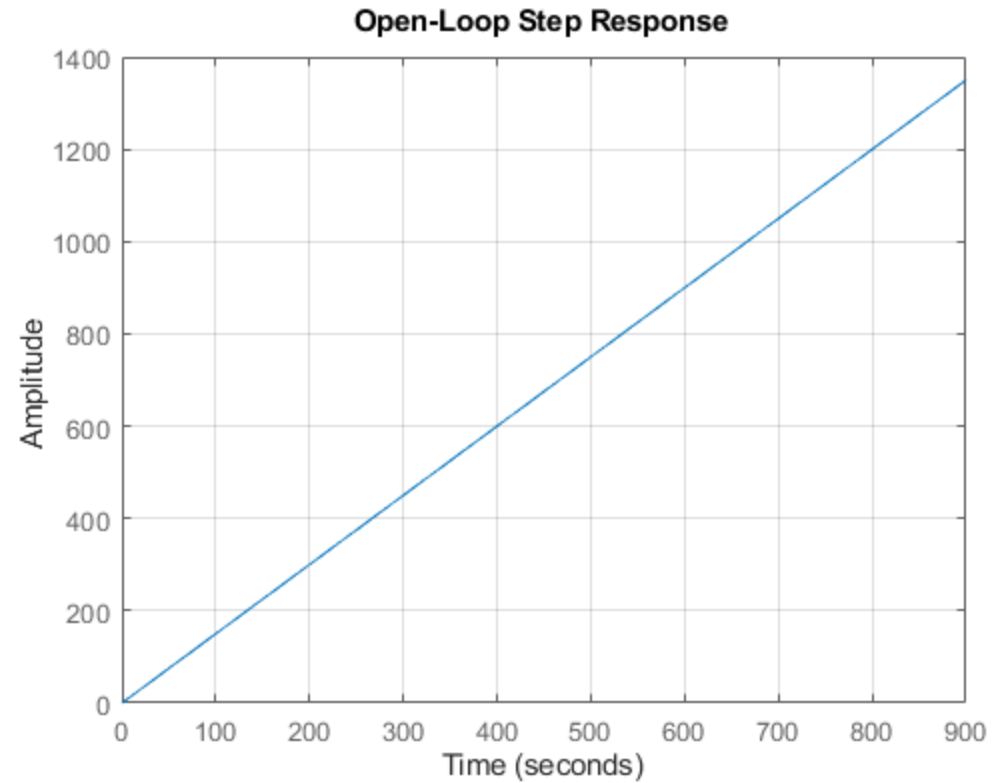
$$u(t) = Ke(t)$$

$$\tan \theta(t) = K(x_{1,desired}(t) - x_1(t))$$

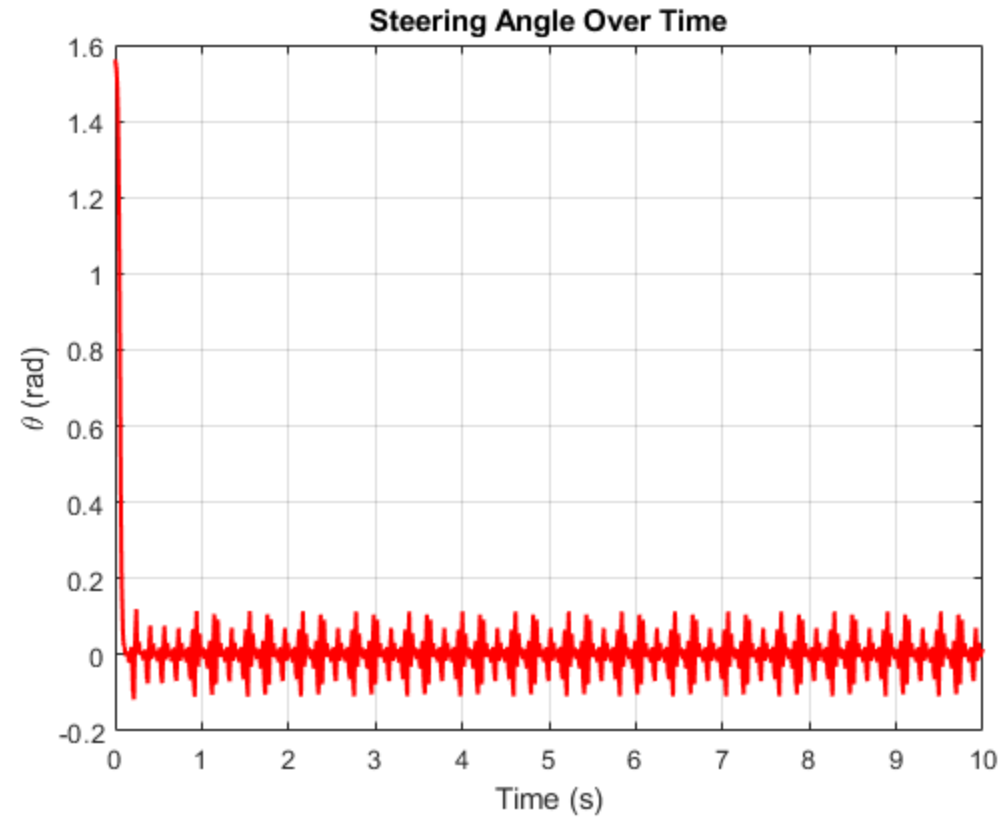
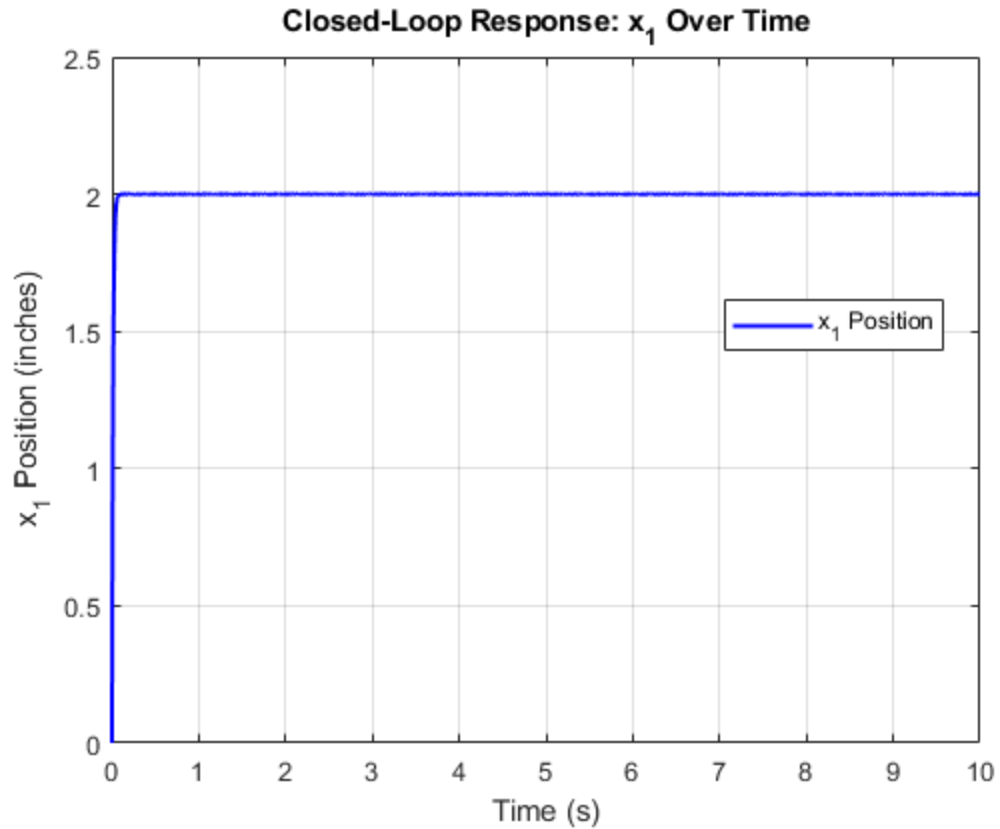
$$\theta(t) = \text{atan}(K(x_{1,desired}(t) - x_1(t)))$$

$$v = r\omega \tan(\text{atan}(K(x_{1,desired}(t) - x_1(t))))$$

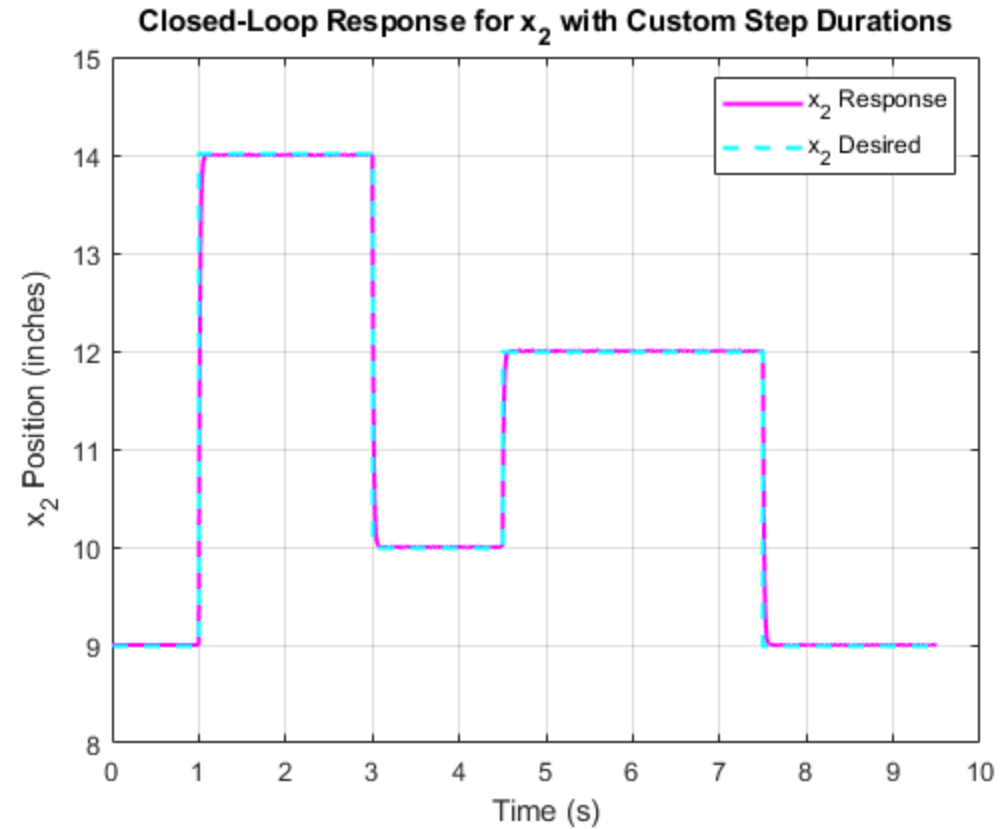
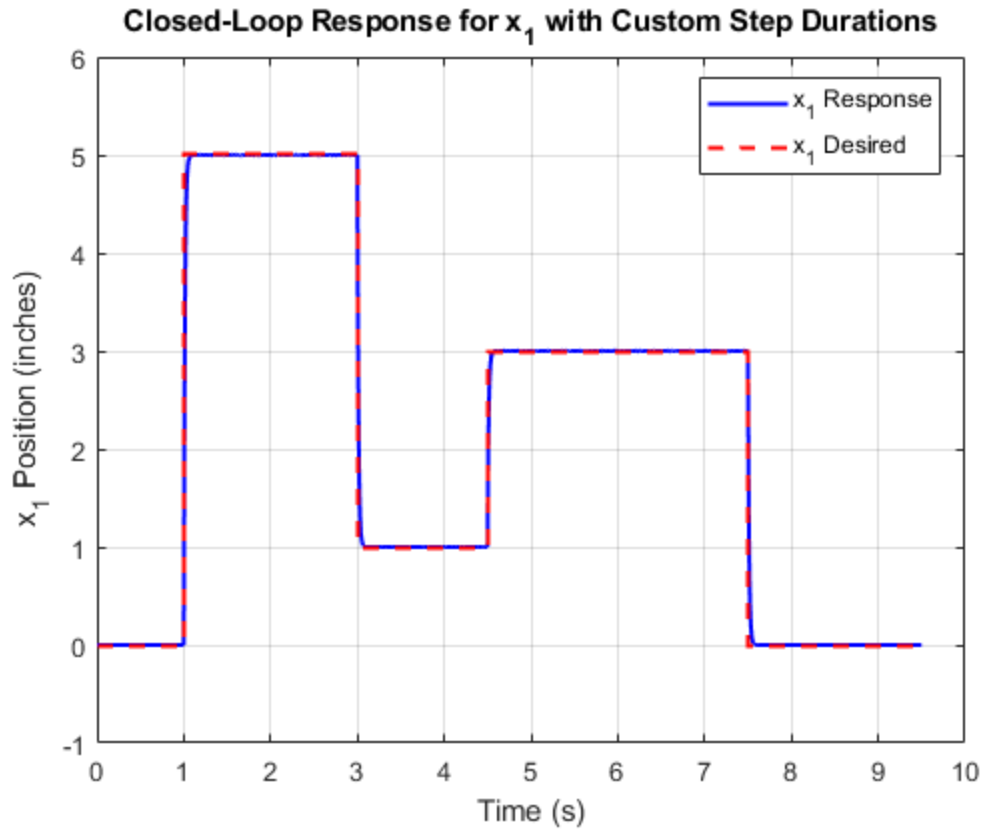
Need For Control



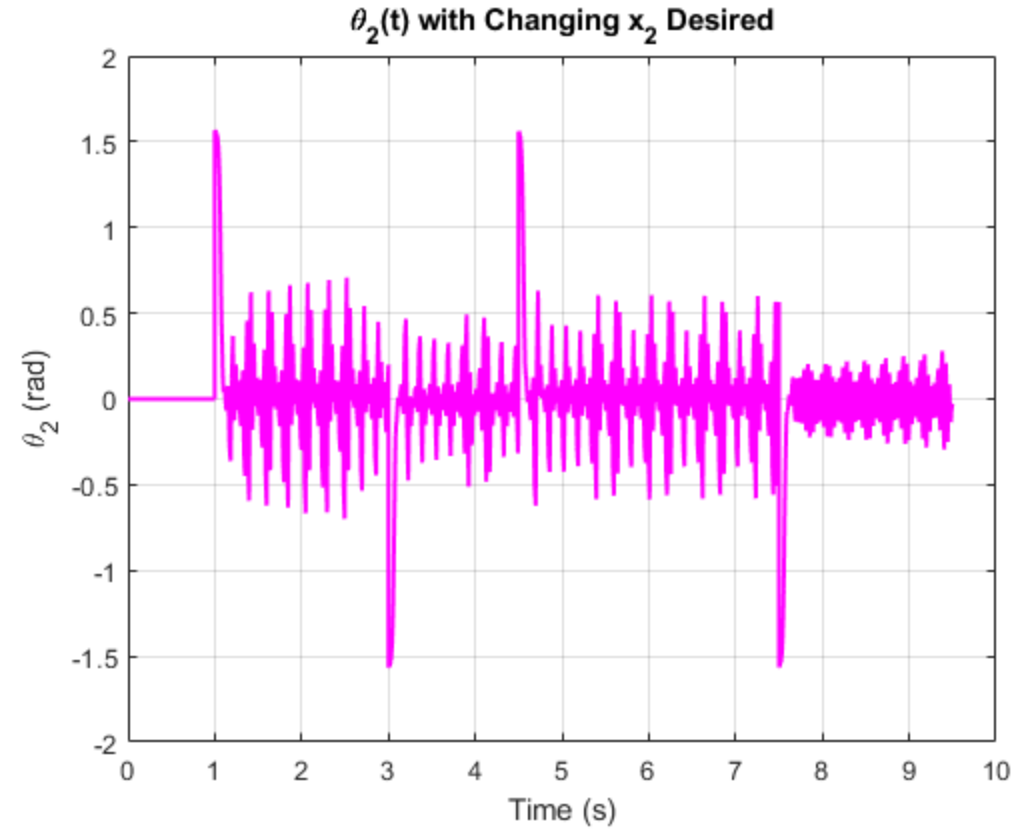
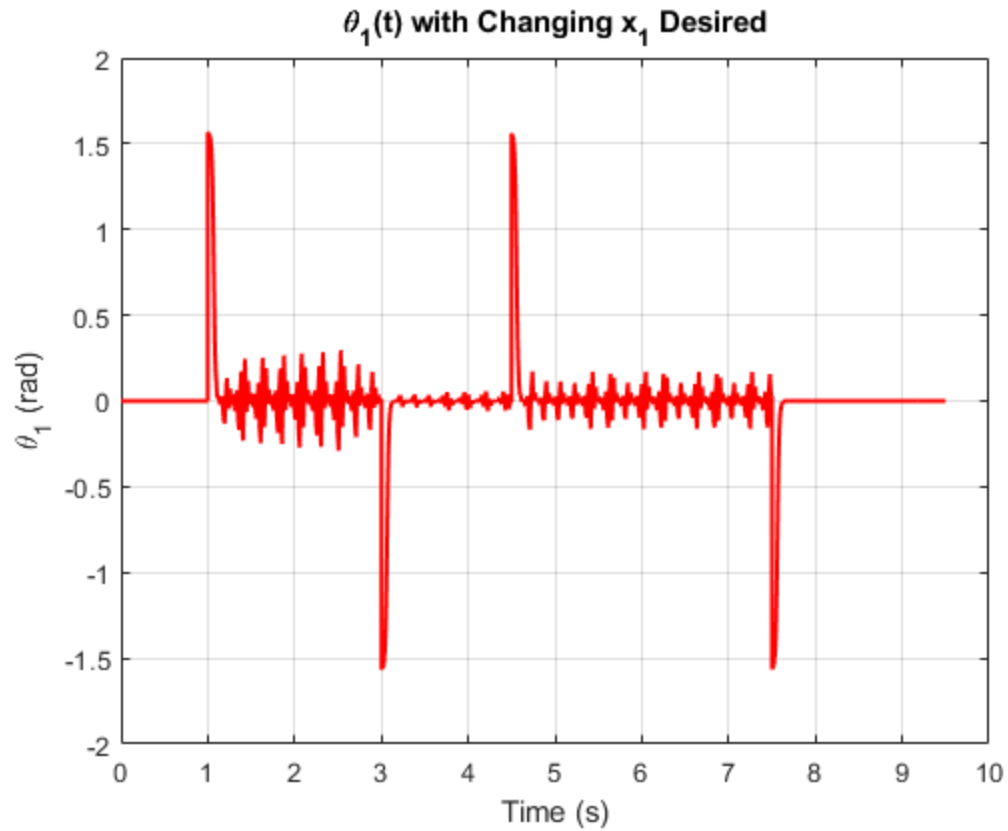
Controller Results – Simple A to B Motion



Sequence of Desired Positions with Tuned Gain

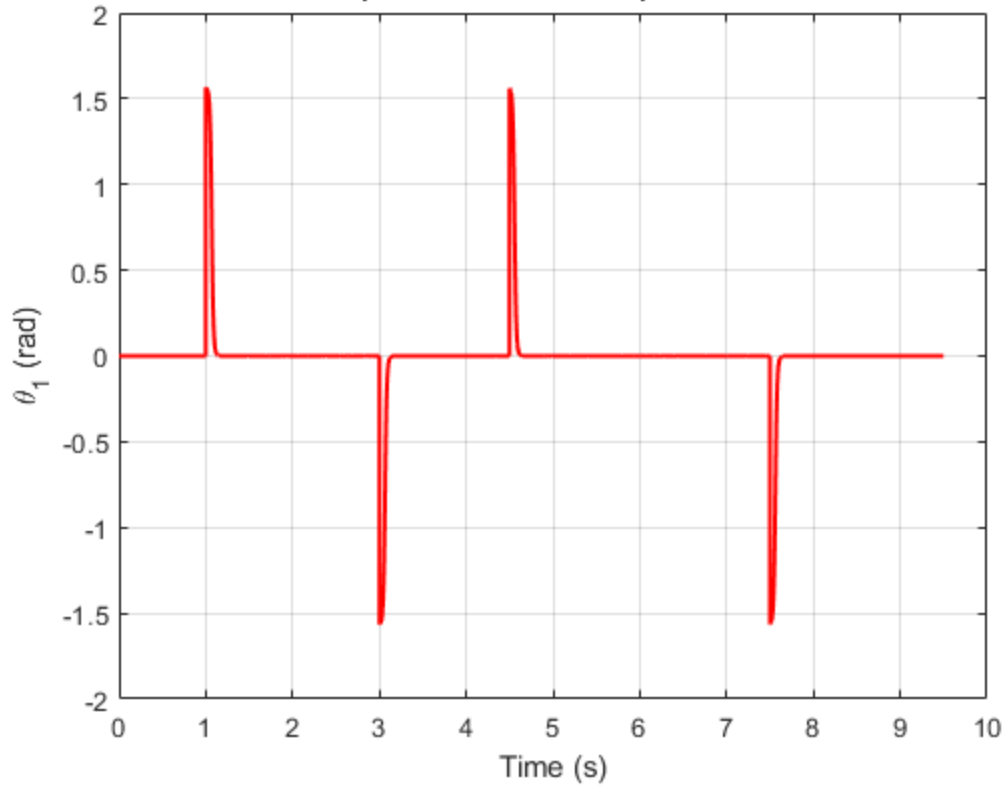


Error Accumulation

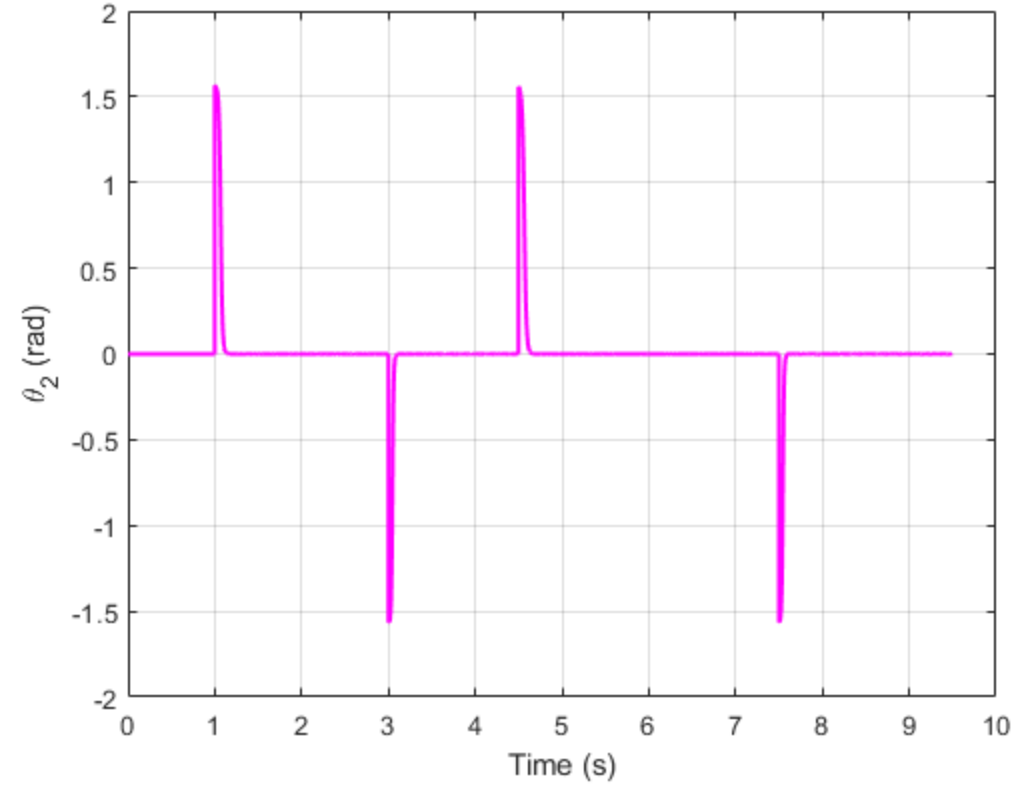


Proposed Solution

$\theta_1(t)$ with Changing x_1 Desired

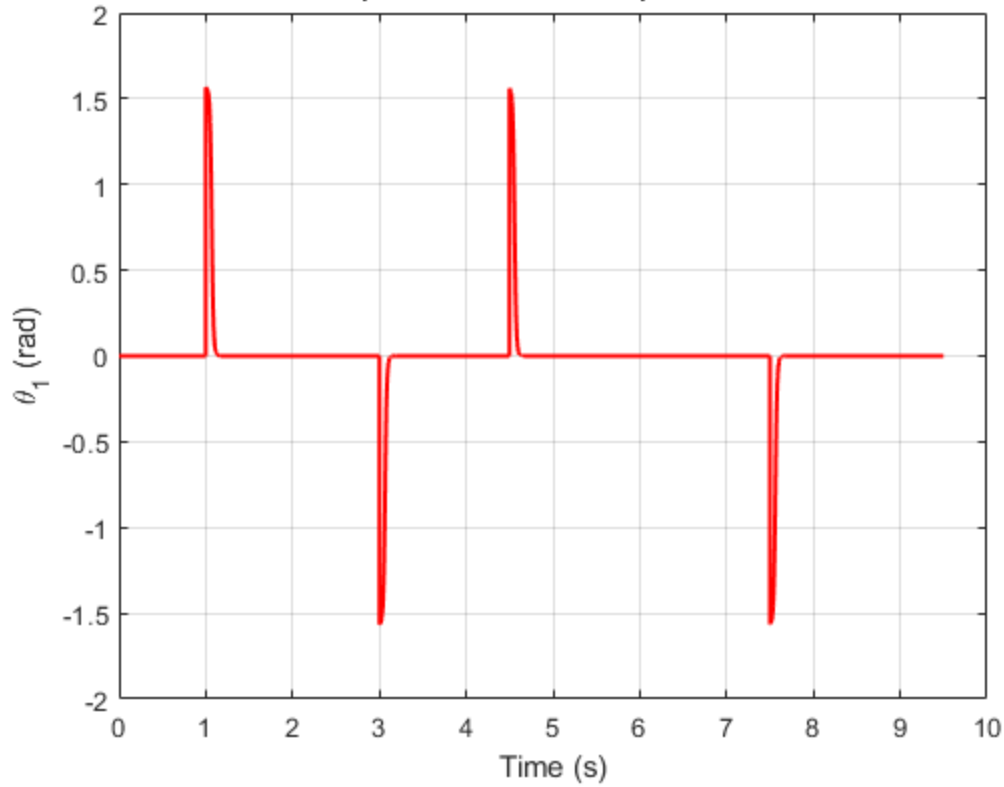


$\theta_2(t)$ with Changing x_2 Desired

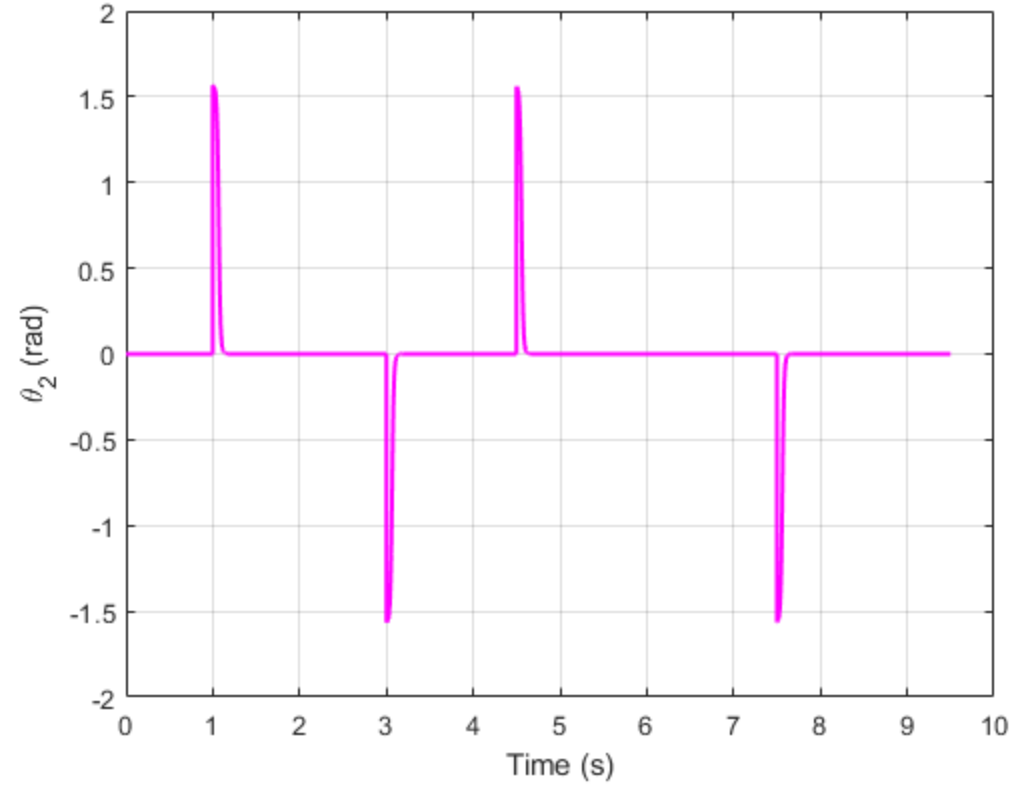


Proposed Solution - Modified

$\theta_1(t)$ with Changing x_1 Desired

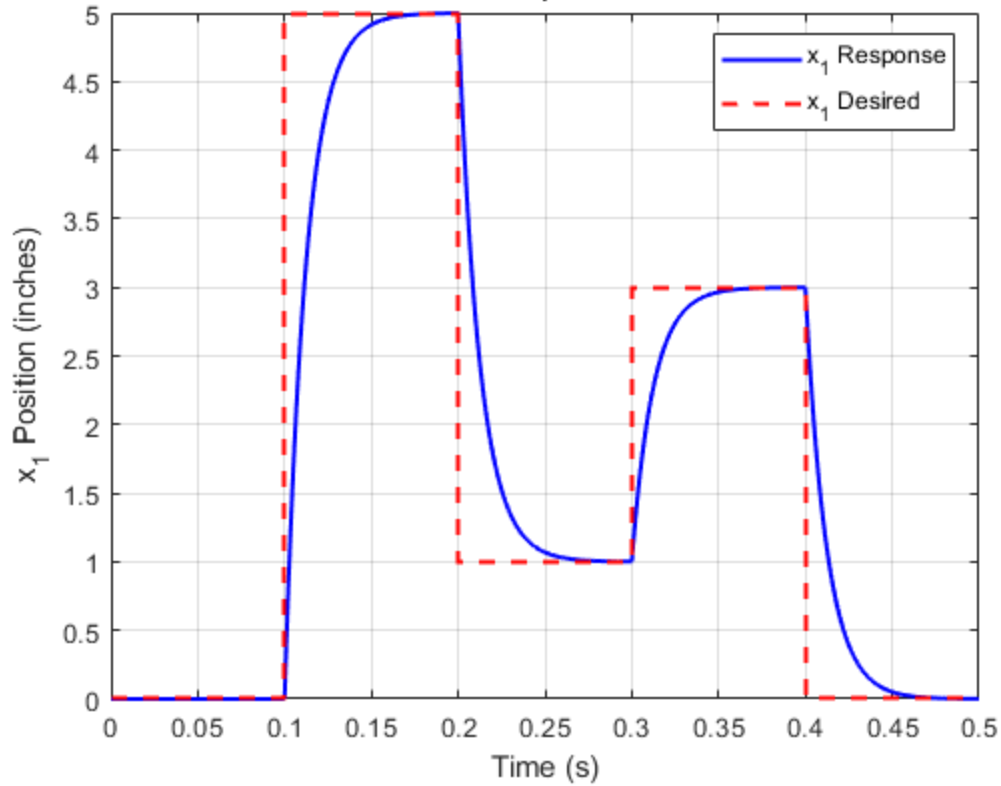


$\theta_2(t)$ with Changing x_2 Desired

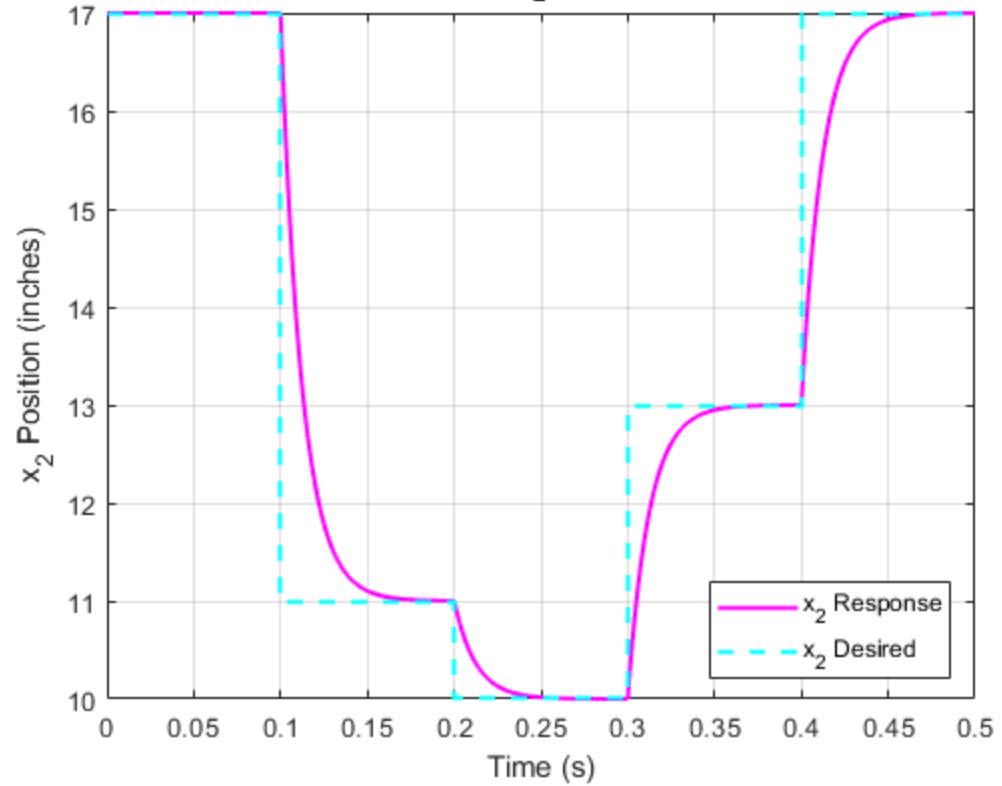


Decreased Time Step Response

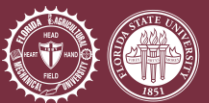
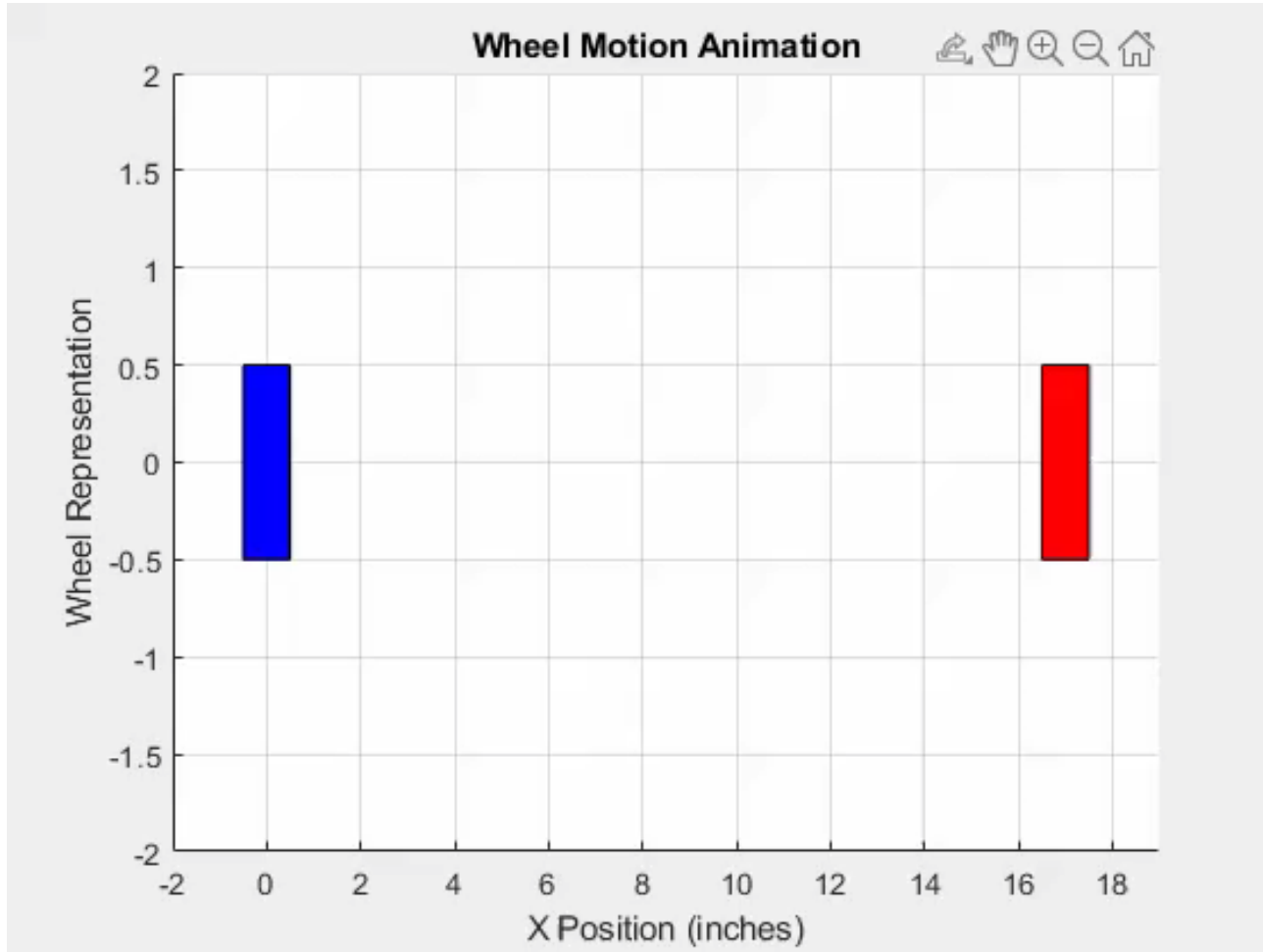
Closed-Loop Response for x_1 with Custom Step Durations



Closed-Loop Response for x_2 with Custom Step Durations

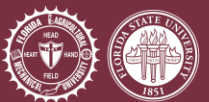


Simple Animation



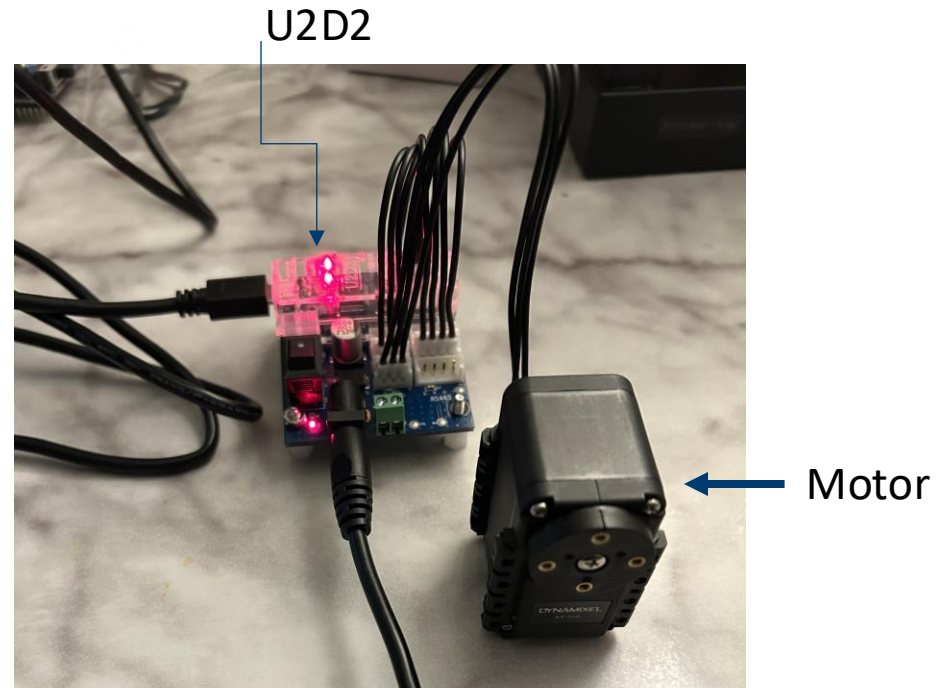
Controls Future Work

- Limit steering angle
- Determine desired x values as a function of end effector kinematics from the new linkage design to create shapes
- Incorporate sensors as x position values for feedback
- Tune gain further based on prototype testing results

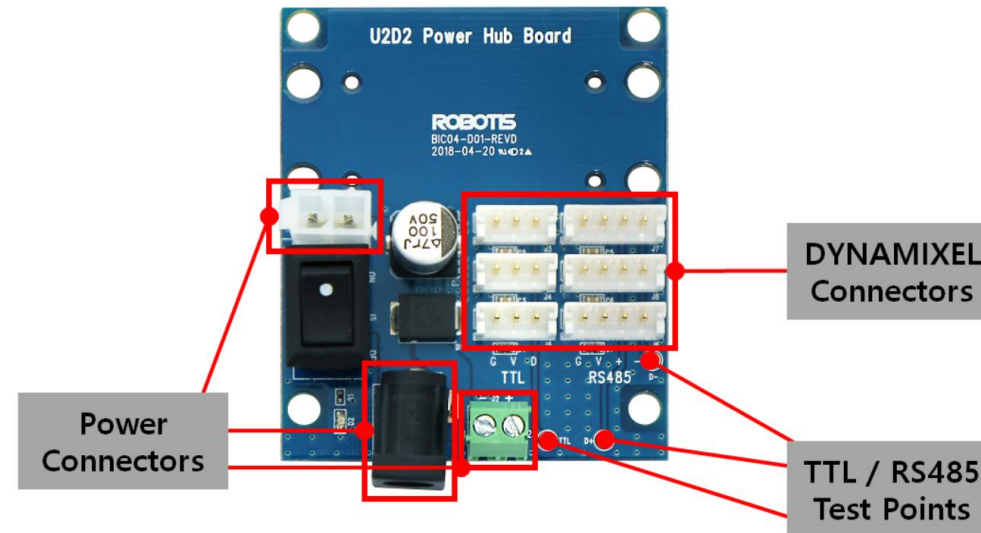


Motor Control

- Successfully controlled the motors and recorded their position vs time.
- Motors were actuated and tested using DYNAMIXEL Wizard software to change IDs and perform basic movements. Components included: U2D2 via USB, Power hub board, AX-12A motor, Wall outlet Power Supply
- “U2D2 is a small size USB communication converter that enables to control and operate DYNAMIXEL with PC.” (Robotis)

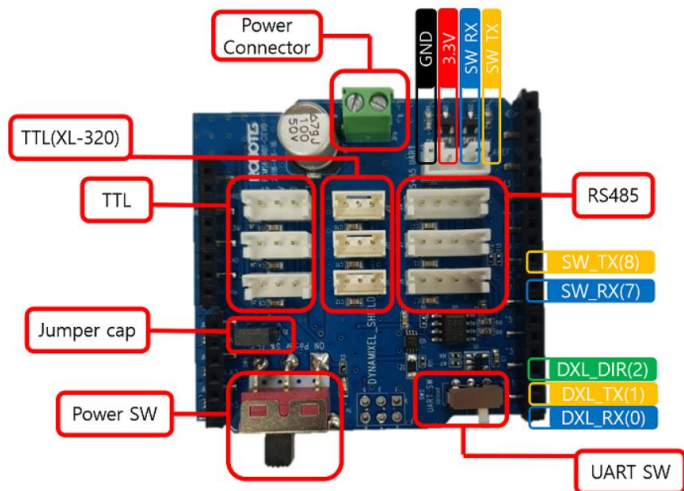


Layout

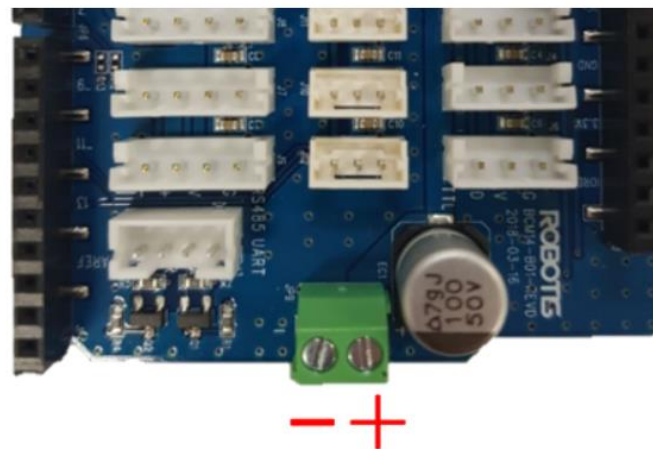


Motor Control: Challenges

- Motor require more power than what Arduino microcontrollers can provide. Arduino is limited to 5V output, while motors require around 11.1V resulting in adequate power.
- Solution: Use an external power supply (12V battery with appropriate adapter) to provide power directly to the shield using the Power Connector rather than Arduino.
- Motors do not actuate when powered solely by Arduino with the DYNAMIXEL shield (component that allows motors to use Arduino).



Graphic layout of DYNAMIXEL SHIELD (ROBOTIS)



Shield



Arduino Mega

Future Works – What To Expect Next Time?

Motion System:

- CVT cylinder driving method selected
- Controller tuning
- Daisy Chaining Motors using Arduino Library Example and proper setup
- Replace use of linear potentiometers with laser sensors

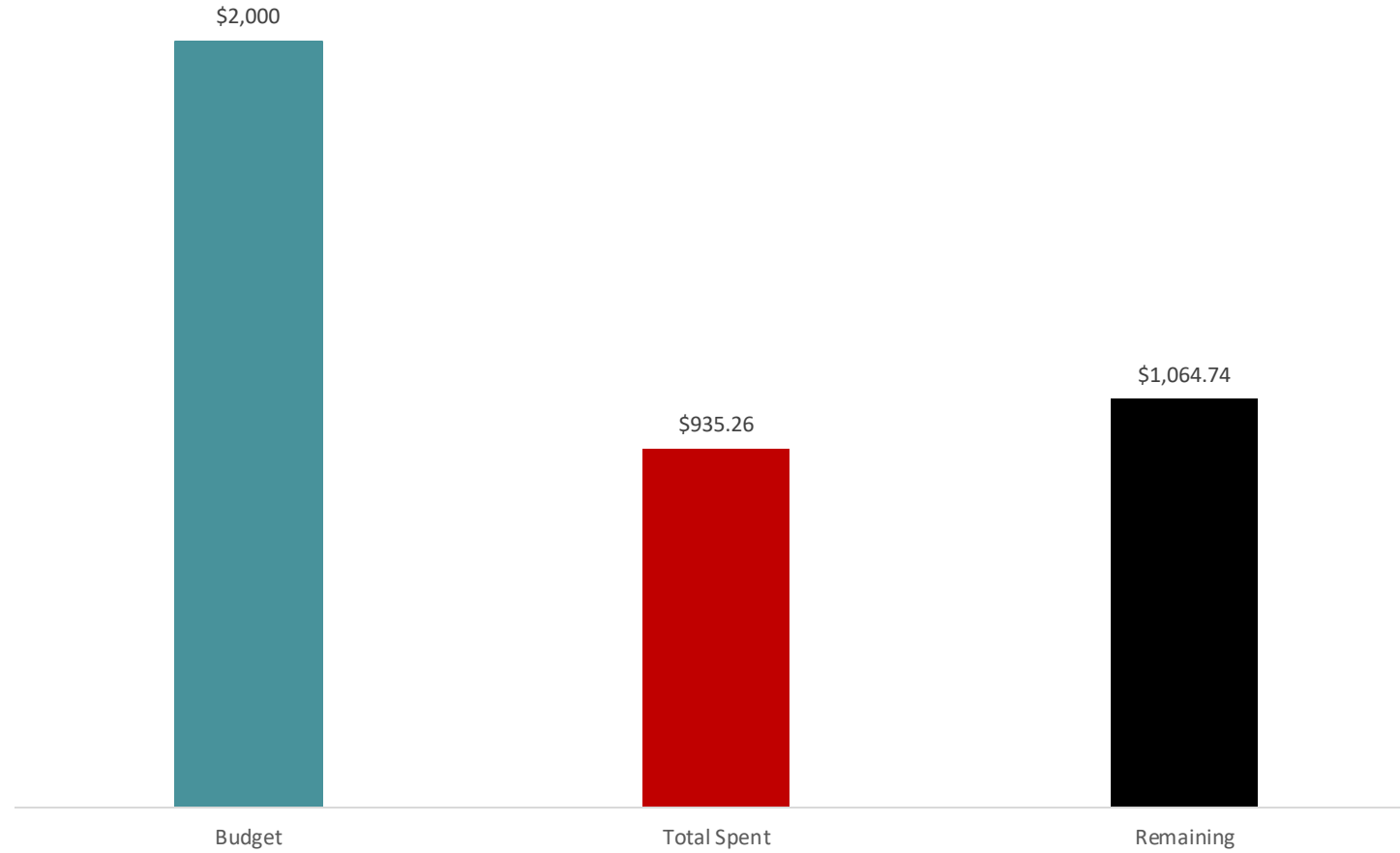
User Interface System:

- Integration with structure and motion systems
- Replace use of LCD screen with OLED screen

Structure System:

- Finalize base design with adjustable preload, sized carriages and linkages, and safeguarding

Thank You



References

Faulring, E. L., Colgate, J. E., & Peshkin, M. A. (2006). *The cobotic hand controller: Design, control, and performance of a novel haptic display*. Department of Mechanical Engineering, Northwestern University.

Faulring, E. L., Colgate, J. E., & Peshkin, M. A. (2005). *A high performance 6-DOF haptic cobot*. Department of Mechanical Engineering, Northwestern University.

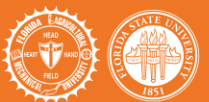
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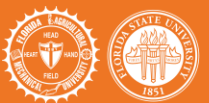
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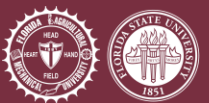
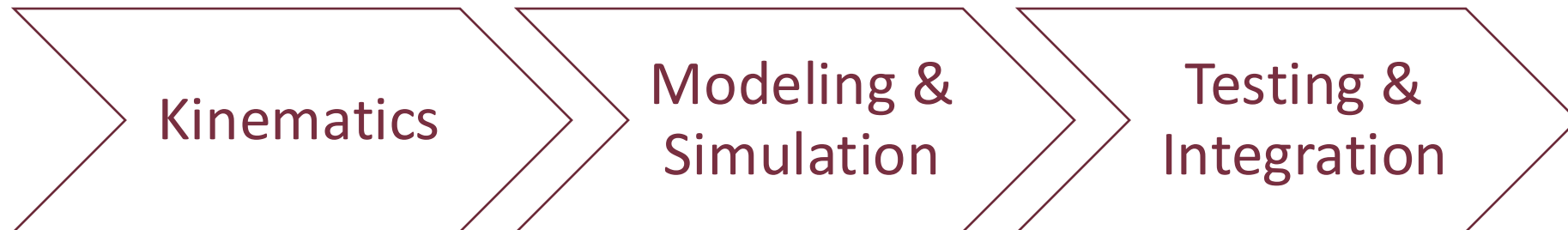
Dynamixel eManual:ROBOTIS. (n.d.). www.robotis.us



Back Up Slides



Future Works – What To Expect Next Time?



References

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https://support.ptc.com/help/wrr/r13.0.1.0/en/index.html#page/wrr/ReferenceGuide/prediction/friction_coefficients.html



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